

FEASIBILITY OF INSTALLING SULFUR DIOXIDE SCRUBBERS
ON STATIONARY SOURCES IN THE
SOUTH COAST AIR BASIN OF CALIFORNIA
VOLUME I: EXECUTIVE SUMMARY

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ABSTRACT

The feasibility and costs of flue gas scrubbing were determined for retrofitting eight selected oil-fired power plants and five industrial sources of sulfur dioxide (SO_2) emissions in the Los Angeles area. Sulfur dioxide scrubbing to achieve the equivalent of 0.05-percent sulfur oil (90 percent SO_2 removal from 0.5 percent sulfur oil) for the utility installations and the removal of approximately 90 percent SO_2 from the other sources were evaluated. The major emphasis on feasibility in this study was for physical installation of the scrubbers.

The power plants selected within the scope of this study represent approximately 80 percent of the fossil fuel-fired power plant generating capacity in the South Coast Air Basin. The SO_2 emissions from the five other sources studied are typical of boilers burning carbon monoxide in flue gas from fluid catalytic cracker units, petroleum coke calcining kilns, and sulfuric acid plants. They currently produce SO_2 emissions equivalent to approximately 18 percent of the emissions now being emitted from the eight power plants.

Technical feasibility for SO_2 removal was established on the basis of the lime-limestone nonregenerable scrubber technology demonstrated in Japan and on units currently being installed and operated in the United States. Other factors such as compatibility with facility operations, space requirements, waste handling, and disposal were examined. Power, water, and flue gas reheating requirements were also addressed.

It was concluded that all of the sites studied can be retrofitted with wet nonregenerable scrubbers capable of removing SO_2 to the levels specified. The degree of difficulty of the scrubber installations varied considerably. Some plants have relatively open areas near the stack, whereas others involve a difficult siting problem. Disposal of scrubber wastes produced from the scrubbers does not appear to present a significant handling problem or impact on existing Class I landfill disposal sites in Los Angeles County.

Capital investment estimates reflecting a range of retrofit complexity and redundancy factors are provided. Corresponding annualized charges in terms of mills per kilowatt hour, dollars per ton SO₂ removed, and dollars per ton product, as appropriate, are reported. The credit resulting from the burning of 0.5 percent sulfur oil by the utilities rather than the 0.25 percent currently in use is also identified.

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Sulfur dioxide scrubber information was provided by the Chemico Division of Envirotech, FMC Corporation, Peabody Process Systems, Pullman Kellogg, Research-Cottrell, and Air Correction Division of UOP, Inc.

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1. INTRODUCTION

The State of California Air Resources Board is evaluating the potential for reducing sulfur dioxide (SO_2) emissions from oil-fired utility power plants and other SO_2 sources in the Los Angeles area. This study has involved assessing the feasibility and cost of retrofitting flue gas scrubbers on utility boilers to achieve SO_2 removal equivalent to use of 0.05 percent sulfur oil (90 percent SO_2 removal from the burning of fuel oil containing 0.5 percent sulfur) and the reduction of SO_2 by approximately 90 percent from existing levels for other sources which include boilers burning carbon monoxide (CO) in the flue gas from fluid catalytic cracker regenerators, petroleum coke calcining kilns, and sulfuric acid units. These objectives are summarized in Table 1.

TABLE 1. SULFUR DIOXIDE REMOVAL OBJECTIVES

Source	Objective
Utility boilers	90 percent removal from combustion of fuel oil with 0.5 percent sulfur
Fluid catalytic cracker carbon monoxide boiler	50 ppm maximum
Petroleum coke calcining kilns	1.5 lb/short ton of coke charged into kiln
Sulfuric acid units	4.0 lb/short ton of product acid

A total of 13 study sites were selected by the research staff of the California Air Resources Board and are identified in Table 2. The eight utility power plants included in this study represent approximately 80 percent of the fossil-fueled electrical power plant generating capacity in the South Coast Air Basin.

TABLE 2. FACILITIES STUDIED

SO ₂ emission source	Agency or company and location
Electrical utility generating stations	Southern California Edison Alamitos El Segundo Etiwanda Huntington Beach Ormond Beach Redondo Beach Los Angeles Department of Water and Power Haynes Valley
Carbon monoxide boiler	Chevron, El Segundo
Petroleum coke calcining kilns	Great Lakes Carbon, Wilmington Martin Marietta Carbon, Carson
Sulfuric acid units	Stauffer Chemical, Carson Collier Carbon, Wilmington

The technical feasibility assessment was based on determining the potential for 90 percent SO₂ removal by flue gas scrubbing. Existing demonstrated technology was considered a significant factor in assessing the SO₂ removal technology of scrubbing processes and their subsequent application to the various specific sites included in the study. Using this criterion, attention was focused on nonregenerative lime-limestone scrubbers that remove 90 percent of the SO₂. Such scrubbers are used extensively in Japan on oil- and some coal-fired boilers and in the United States on coal-fired units. The more complex and less developed regenerable processes were to be considered in the event that 90 percent removal efficiency was not achievable by means of first-generation, nonregenerable technology or if problems arising from the quantity or disposal of wastes produced from the nonregenerables made their application impractical.

The study involved a number of facets, including the following:

- a. Assessment of scrubber technology
- b. Characterization of the sites
- c. Identification and assessment of scrubber system operation
- d. Determination of site-specific feasibility and costs.

The approach taken to assess feasibility of installing SO₂ scrubbers is summarized in Table 3.

Assessment of the technology potential for the nonregenerable systems was based on evaluation of the results reported for the operational installations on numerous oil- and some coal-burning boilers in Japan and coal-burning units in the United States. Information developed through discussions with personnel knowledgeable of the details of the Japanese processes and those familiar with U.S. technology was used to augment the published data. Similar contacts were made with regard to the smaller scrubber units applicable to the industrial, nonutility installations.

For the data needed to evaluate each Los Angeles study site, information was derived from conferences with cognizant technical personnel from the various companies involved. The responses of various organizations

TABLE 3. SULFUR DIOXIDE SCRUBBER -- FEASIBILITY
STUDY APPROACH

Major areas of investigation	Specific tasks
Assess scrubber technology	Determine sulfur dioxide removal efficiency Assess scrubber operability
Characterize power plants and industrial sites	Make on-site visits Analyze responses to questionnaires defining plant characteristics and layout Review plot plans and aerial photographs
Identify and assess scrubber system operation	Determine ability to reduce sulfur dioxide to required levels Identify operating characteristics Quantify operating requirements Identify waste disposal impacts
Determine site-specific feasibility and costs (capital, operation and maintenance and annualized)	Obtain sizing, operating, and cost data from scrubber suppliers--Chemico, FMC (industrial), Peabody (industrial), Pullman Kellogg, Research Cottrell (utility and industrial divisions), and UOP Consider effects of retrofit complexity and equipment redundancy on scrubber installations Include cost benefits of using 0.5 percent sulfur oil instead of current 0.25 percent oil Relate scrubber operating costs to selling price of product

to questionnaires developed by The Aerospace Corporation were also used. Based on scrubber supplier inputs and published data, scrubber system requirements and operating conditions were identified and quantified. These included scrubber reagent, fresh water, power, and wastes produced by each of the sites. Further, by utilization of site plot plans, aerial photographs, and equipment sizing information provided by various scrubber suppliers, layout sketches were made showing size, location, and orientation of the scrubber modules, lime storage facilities, and the waste handling and holding facilities. In addition, major impacts or modifications to existing facilities as determined by a review of the plot plans and site visits were identified.

Based on budget-type information provided by the scrubber manufacturers for grass-roots installation, capital cost estimates for retrofitting the sites were prepared as a function of several levels of complexity. The costs associated with a number of levels of equipment redundancy were determined. Annualized charges were defined which included capital charges, scrubber system operation, and waste disposal. Costs associated with plant or unit shutdown for installation of scrubber equipment were not included.

2. SUMMARY AND CONCLUSIONS

The study was oriented towards determining the feasibility of installing SO₂ scrubbers on selected utility boiler and industrial emission sources in the Los Angeles area. Four basic considerations in assessing feasibility in this study were addressed:

- a. Technical feasibility of 90 percent SO₂ removal
- b. Scrubber process definition
- c. Feasibility of scrubber system installations at selected sites
- d. Cost of site-specific capital equipment, total capital investment, and annualized costs.

Thirteen sites, which included six Southern California Edison (SCE) and two Los Angeles Department of Water and Power (DWP) generating stations (Table 4) and five industrial boiler and process sites were studied. The latter included a boiler burning carbon monoxide (CO) in the flue gas from a catalytic cracker regenerator, petroleum coke calcining kilns, and sulfuric acid units (Table 5). In general, the SO₂ removal requirement used in the study was a nominal 90 percent removal. The current emissions and the specific SO₂ removal requirements to meet study objectives for the various sources are defined in Table 6.

2.1 TECHNICAL FEASIBILITY OF SO₂ CONTROL REQUIREMENTS

As a result of this study, it was concluded that 90 percent removal of SO₂ flue gas, originating from oil-fired utility boilers and from industrial processes, can be accomplished on the basis of existing nonregenerable scrubbing technology. Consistent removal efficiencies of 90 percent or greater have been demonstrated in Japan, primarily on oil-fired and some coal-fired boiler installations. Currently, scrubber units are being installed on coal-fired units in the United States to meet 90 percent SO₂ control requirements. Removal efficiencies in excess of 90 percent have been demonstrated with some scrubbers installed on industrial combustion and process sources of SO₂ in the United States.

TABLE 4. ELECTRICAL UTILITY FACILITY CHARACTERISTICS

Electric utility generating station	Generating capacity, MW	No. of units	Average capacity factor, 1976
Southern California Edison			
Alamitos	1,950	6	0.442
El Segundo	1,020	4	0.444
Etiwanda	904	4	0.498
Huntington Beach	870	4	0.434
Ormond Beach	1,600	2	0.454
Redondo Beach	1,602	8	0.15 ^a /0.451
Los Angeles Department of Water and Power			
Haynes	1,633	6	0.667
Valley	526	4	0.158 ^b
Total	10,105	38	0.424 ^c

^a0.15 applies to Units 1 through 4; 0.451 applies to Units 5 through 8

^bUnits 1 and 2 were for 1975

^cWeighted average (excluding a and b)

TABLE 5. PETROLEUM AND CHEMICAL PROCESSING
FACILITY CHARACTERISTICS

Installation	Unit size, tons/day	No. of units
Carbon monoxide boiler -- Chevron	a	1
Petroleum coke calcining kilns		
Great Lakes Carbon	900 (ea)	3
Martin Marietta Carbon	960	1
Sulfuric acid units		
Stauffer Chemical	300 (ea)	2
	200	1
Collier Carbon	450	1
Total	--	9
^a Not available -- boiler rated at 250,000 lb/hr steam		

TABLE 6. SULFUR DIOXIDE EMISSION CONTROL CONDITIONS
CONSIDERED IN THIS STUDY

Electrical utilities and industrial sources	Current		Objectives	
	Status	Approximate emissions, ppm	Removal by scrubber, percent	Emissions
Electrical utility boilers -- DWP and SCE units	Sulfur content in fuel oil not to exceed 0.25 percent	150	90 from combustion of oil with 0.5 percent sulfur	30 ppm (approx.)
Carbon monoxide boiler -- Chevron	SO ₂ content of flue gas emissions is a function of crude being processed, in the range of 150 to 400 ppm	225 (avg)	88 for 400 ppm inlet	50 ppm maximum
Petroleum coke calcining kilns Great Lakes Carbon	Emissions are function of crude: currently 300 to 380 ppm (approx. 1.3% sulfur in coke)	300 (wet)	88 for normal production rates and 300 ppm	1.5 lb SO ₂ per short ton of coke charged into kiln
Martin Marietta Carbon	2.3 to 2.5 percent sulfur crude	700 (wet)	93 for 2.5 percent sulfur crude	
Sulfuric acid units Stauffer Chemical	300 to 500 ppm	400	33 for Units 1 and 2 66 for Unit 3	4.0 lb SO ₂ per short ton of product
Collier Carbon	350 ppm	400	15 (ave.)	

Since a significant data base exists to support the SO_2 removal capability of the lime-limestone nonregenerable process for the large utility installations, this process was selected for further evaluation and quantification. Nonregenerable lime scrubbing, rather than limestone, was chosen for process definition and quantification (Figure 1) because lime has smaller space and handling requirements. Consideration of limestone would not result in any fundamental changes to the results of this study because basic scrubber tower sizes are nominally the same for both, being determined by the volumetric flow and spatial velocity of the flue gas through the tower. However, for a given amount of SO_2 removal, approximately 100 percent more limestone (CaCO_3) reagent, by weight, would be required in contrast to lime (CaO) because of chemical differences in the reagent and the slightly lower limestone utilization. The limestone process would also require pulverizing facilities, which are not needed with lime, and approximately 5 percent more scrubber waste would be produced if limestone were used.

Because of the limited area available at certain sites and the experience in applying the double alkali process to industrial use, the latter process (Figure 2) was considered, in addition to lime scrubbers for the smaller, nonutility installations in this study.

Electrical power, water, and flue gas reheating requirements were defined. A generalized schematic summarizing the various operating conditions is given in Figure 3, and total quantities are provided in Table 7 for all sites studied.

Filtered scrubber waste totalling approximately 328,000 tons or 163 acre-feet would be produced annually by the eight utility sites. The industrial sources studied would add approximately 14 percent. The disposable waste from the lime scrubbers was estimated to contain 72 percent solids subsequent to vacuum filtration, the latter being accomplished at the scrubber site. Use of trucks to transport the waste to two Class I, geographically appropriate disposal sites in Los Angeles County was determined to be feasible with

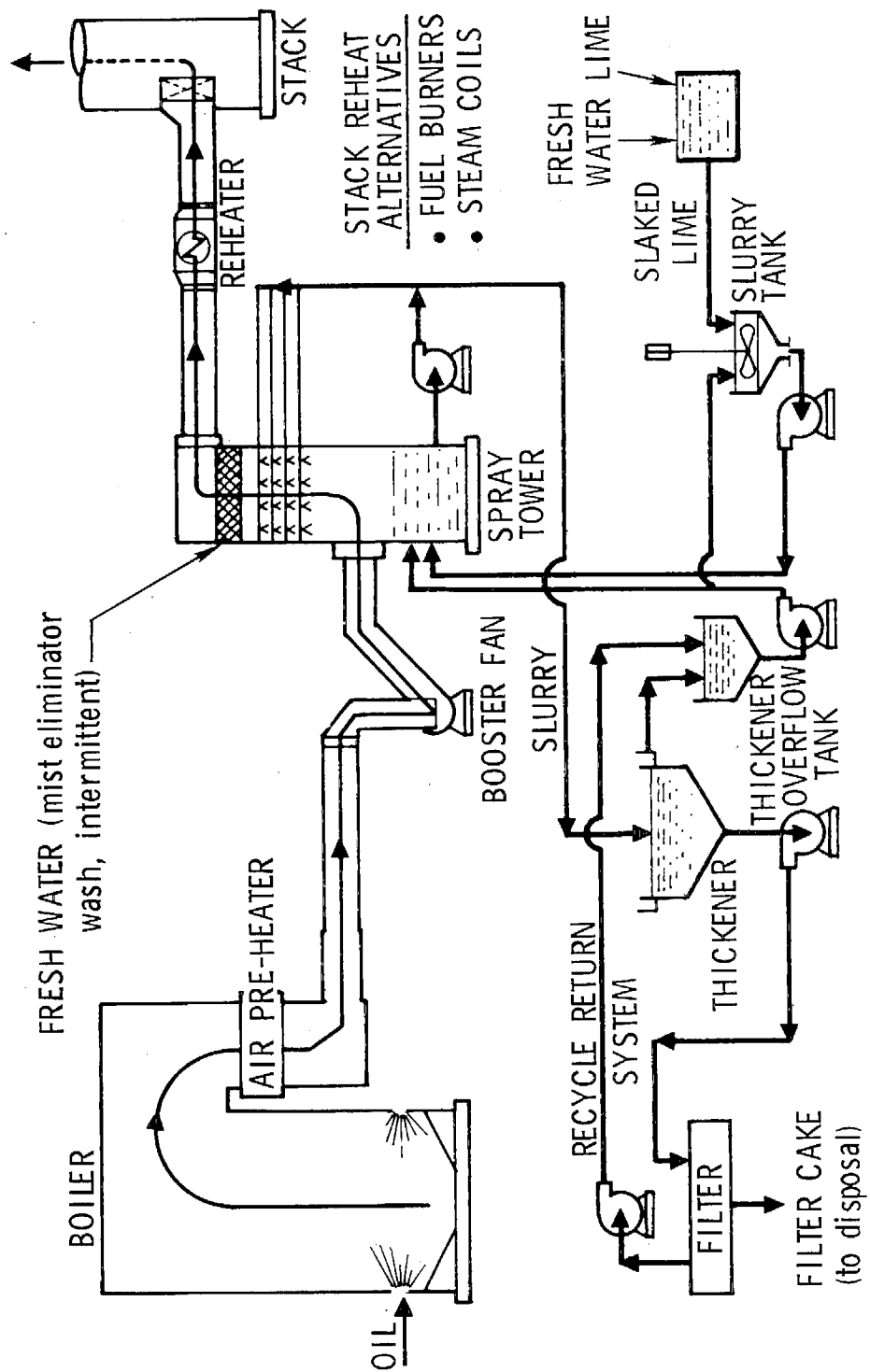


Figure 1. Lime scrubbing schematic

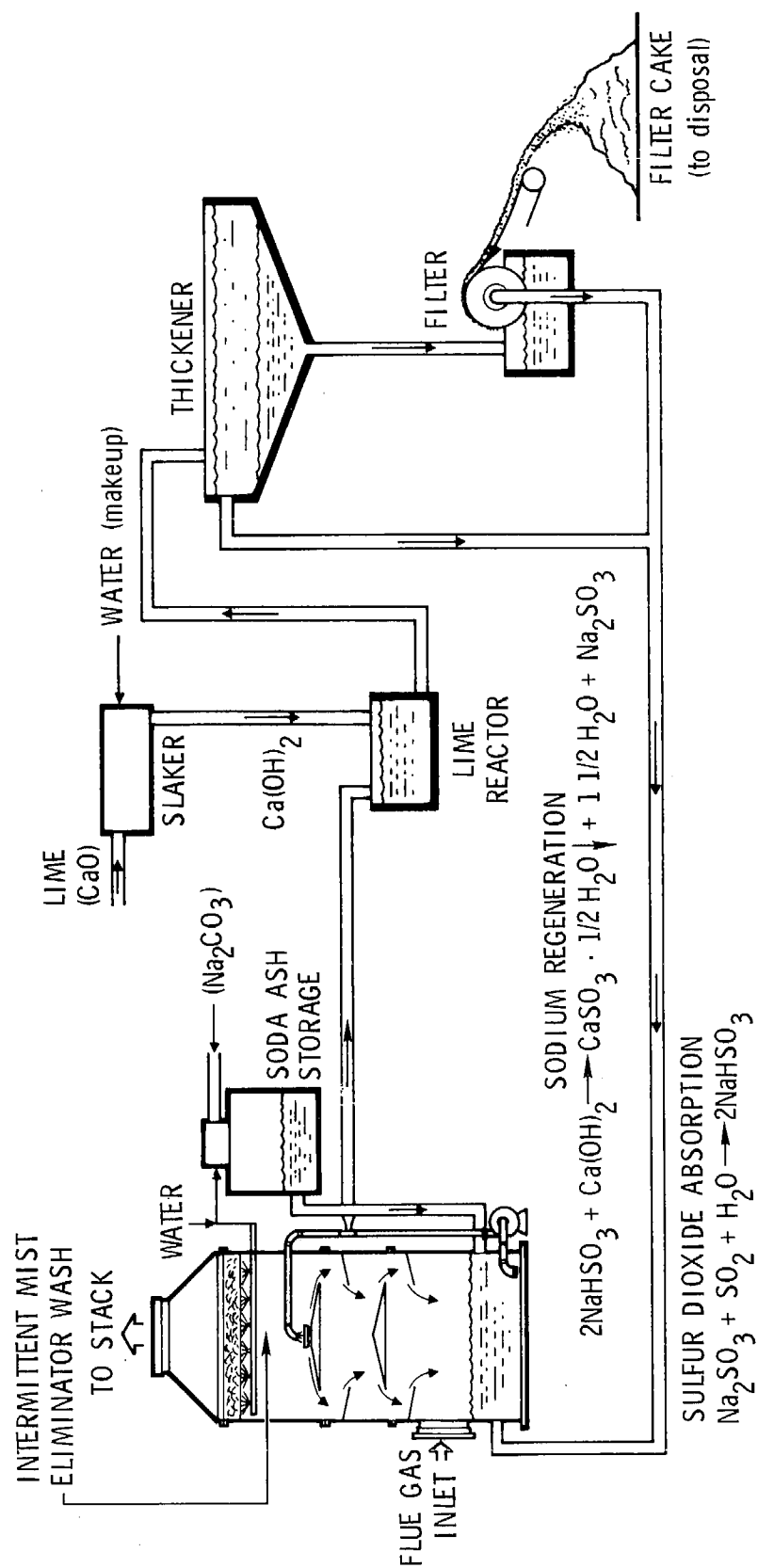


Figure 2. Double alkali process schematic

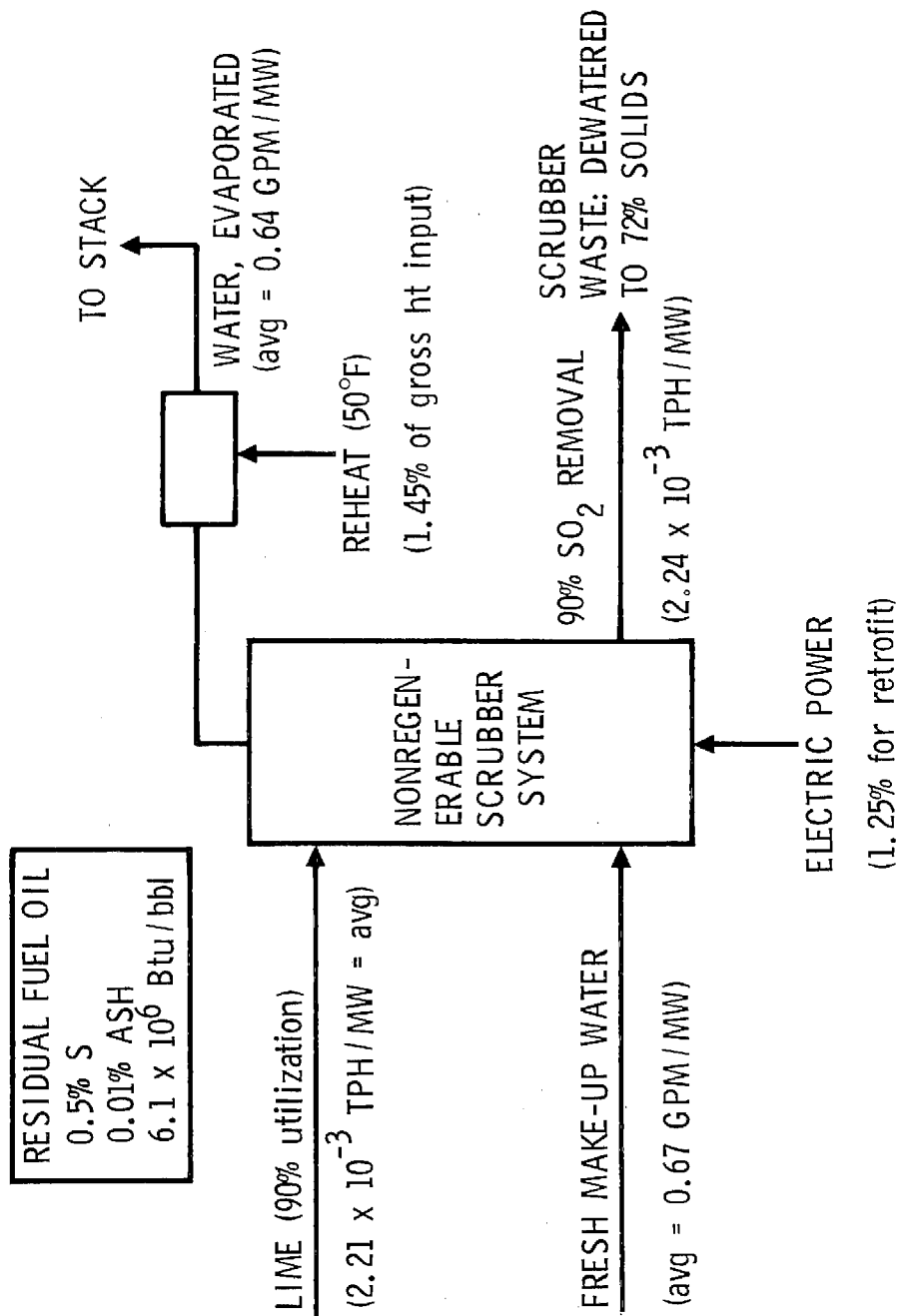


Figure 3. Generalized sulfur dioxide scrubber parameters -- electric utility boilers

TABLE 7. QUANTIFICATION OF SCRUBBER SYSTEM PARAMETERS

Parameter	Utility	Industrial process
Number of sites	8	4 ^a
Total generating capacity, MW	10,105	Not applicable
Number of units retrofitted	38	8
Annual operation		
Capacity factor	0.424	--
Hours	--	8,200 (typical)
Sulfur dioxide removed annually, tons	91,100 ^b	9,340
Scrubber waste produced annually		
Tons	327,800	44,500
Acre-feet	163	23.1
Annual lime consumption, tons	89,000	10,500
Current daily fresh water use		
Gallons	4,510,000	1,100,000
Increased consumption--all units, percent	37	22
Annual electric power required, KWh	469×10^6 ^c	44×10^6
Annual reheat requirement (50° F)	1.45 ^d	13.0×10^{10} Btu
^a Fifth site not applicable -- see discussion in Section 4.3.2 ^b 90 percent sulfur dioxide removal; fuel oil burned contains 0.5 percent sulfur ^c Equivalent to 1.25 percent of power generated ^d Percent of gross heat input		

nominal impact on the remaining life of the disposal sites. An operating cost of about \$7.14 per ton of disposable dewatered waste was estimated. The conversion of wastes to a useable product and the potential marketability of waste products were not within the scope of this study.

2.3 FEASIBILITY OF SCRUBBER INSTALLATIONS

Feasibility of SO₂ scrubber installation was based on factors defined for this study and are summarized in Table 3. For the eight utility sites studied, retrofitting of a total of 38 generating units, 41 boilers, with vertical, nonregenerable scrubbers was determined to be feasible on the basis of operating information furnished by the utilities, site visits, plot plans, aerial photographs, and scrubber size and operating information provided by scrubber suppliers. In general, the availability of land and space near the boiler was of primary importance in siting the scrubbers and in determining the resultant complexity of installation (Table 8). While other equipment such as horizontal nonregenerable scrubbers or processes such as those capable of producing sulfur or sulfuric acid might also be feasible at certain utility sites, the potential optimization, if any, of processes or equipment was not an objective of this study.

For the catalytic cracker carbon monoxide boiler and the process industries installations, retrofitting with scrubbers was found to be feasible (Table 9). Both nonregenerative lime and double alkali processes were considered. Lime scrubbers that are commercially available for industrial applications from a major U.S. supplier that was contacted in this study are provided in discrete modular sizes. In one instance, multiple scrubber units were required and could not be accommodated because of space limitations. In that case, a double alkali system with a single scrubber tower was considered.

One industrial site, the Collier Carbon sulfuric acid plant, Wilmington, California, is operating an ammonia scrubber, which reduces SO₂ emissions to approximately 4.7 pounds of SO₂ per ton of product. In order to meet the 4.0-pound value, 15 percent SO₂ removal would be

TABLE 8. ENGINEERING ASSESSMENT OF SITE-SPECIFIC
INSTALLATION FEASIBILITY -- UTILITIES

Generating station	Capacity, MW	No. of boilers	No. of scrubbers	Retrofit installation ^a complexity ^a
Southern California Edison				
Alamitos	1950	6	10	Moderate
El Segundo	1020	4	8	Difficult
Etiwanda	904	4	6	Nominal
Huntington Beach	870	4	4	Nominal
Redondo Beach	1310	4	6	Difficult
	292	7	2	Difficult
Ormond Beach	1600	2	8	Moderate
Los Angeles Department of Water and Power				
Haynes	1633	6	10	Moderate
Valley	526	4	4	Nominal
^a Based on availability of space and complexity of installation				

TABLE 9. ENGINEERING ASSESSMENT OF SITE SPECIFIC
INSTALLATION FEASIBILITY -- INDUSTRIAL SITES

Installation	Unit or plant rating	No. of units	No. of scrubbers ^d	Installation complexity ^a
Carbon monoxide boiler -- Chevron	250,000 lb/hr steam	1	2	Nominal
Petroleum coke calcining kilns				
Great Lakes Carbon	2700 tons/day raw coke	3	3	Difficult
Martin Marietta Carbon	960 tons/day raw coke	1	1	Nominal
Sulfuric acid units				
Stauffer Chemical	800 tons/day sulfuric acid	3	3 ^e	Moderate
Collier Carbon	450 tons/day sulfuric acid	1	1 ^b	Nominal ^c
^a Primarily based on availability of space ^b Existing ^c If additional scrubber is required; see discussion in Section 4.3.2 ^d Double alkali process ^e Nonregenerable lime process				

required. It was determined that the existing scrubber could be operated to meet the study objective of 4.0 pounds. However, some questions were raised about the possibility of increasing plume opacity above current allowances. The scrubber supplier indicated that techniques could be employed to decrease plume opacity if it occurred. In addition, space is available in the event opacity were a problem and a nongenerable scrubber is required.

Capital, operating, and annualized cost estimates were determined. Capital investment estimates utilized generic scrubber equipment costs for new installations provided by scrubber suppliers. Total capital investment estimates were computed on the basis of a range of retrofit and redundancy factors. Owner total capital investment costs for the utility scrubber installations ranged from an average of \$118 to \$154 per kilowatt, with an overall average of \$135 per kilowatt (late 1977 dollars) (Table 10a). The lower figure includes a 10 percent factor for redundancy and retrofit complexity and represents the lower limit anticipated for a non-complex installation with limited redundancy. The higher value includes significantly greater factors, i. e., 40 percent each. The 10 to 40 percent installation complexity range is estimated as being the range that would encompass those items that cannot be specifically defined unless a detailed engineering study were conducted for each site. They may include relocating underground and surface facilities and installation of complex duct work from the scrubber to existing stack entry locations if a detailed design study were to indicate it was practical or to extend the ducting to new stacks. In estimating capital equipment costs for this study, costs of new stacks were included. These costs are itemized for each utility site in Section 4.5.1.1 and are summarized in Table 11.

The total capital investment for the industrial process scrubbers does not lend itself to a generalization such as dollars per kilowatt. Therefore, the average costs for each site are indicated in Table 11, and the range of retrofit costs in Table 10b.

Average annualized costs were calculated as 8.8 mills/kWh, or \$3612 per ton of SO₂ removed, for a 20-year expected life for the utility scrubber systems, including 0.062 mills/kWh for scrubber waste transport and disposal. Considering the cost benefit derived from the use of oil with 0.5 percent sulfur, which is approximately \$0.70 per barrel less than the fuel with 0.25 percent sulfur which is now in use, the operating cost would

TABLE 10a. TOTAL CAPITAL INVESTMENT FOR UTILITY INSTALLATIONS:
RETROFIT AND REDUNDANCY FACTORS INCLUDED

Late 1977 dollars

Installation	Generating capacity, a MW	Average capacity factor, 1976	Grass roots installation, owner's capital investment, \$/kW ^b (average)	Total capital investment			
				Maximum ^c \$/kW	Minimum ^c \$/kW	Average ^c \$/kW	Average ^d \$ (000, 000)
Southern California Edison							
Alamitos	1,950	0.442	91.3	138.1	103.4	120.6	235.2
El Segundo	1,020	0.444	107.4	161.5	120.9	161.5 ^e	164.7 ^e
Etiwanda	904	0.498	109.5	164.7	123.3	143.9	130.1
Huntington Beach	870	0.434	108.6	163.3	122.3	142.7	124.2
Ormond Beach	1,600	0.454	92.7	139.4	104.4	121.8	194.9
Redondo Beach	1,310	0.451 ^f	100.0	150.4	112.6	150.4 ^e	197.0 ^e
	292	0.15					43.9
Los Angeles Department of Water and Power							
Haynes	1,633	0.667	89.4	134.4	100.7	117.5	191.9
Valley	526	0.158	117.4	176.6	132.3	154.3	81.2
Average	--	--	102.01	153.5	115.0	134.9 ^g	--

^aTotal generating capacity 10,105 MW

^bSee Table 63

^cMaximum capital investment includes +40 percent for retrofit and +40 percent for redundancy

Minimum capital costs include +10 percent for retrofit and +10 percent for redundancy

Average capital costs include +25 percent for retrofit and +25 percent for redundancy

^dTotal capital investment is \$1.363 billion

^eMaximum retrofit and redundancy factors used because of installation complexity

^f0.451 applies to Units 5 through 8; 0.15 applies to Units 1 through 4

^gWeighted average

TABLE 10b. INDUSTRIAL PROCESS SO₂ SCRUBBER CAPITAL INVESTMENT

Late 1977 dollars

Installation and No. of units	Supplier capital cost estimate, \$(000,000)	Grass roots installation, owner's total capital investment, \$(000,000)	Total capital investment, \$(000,000)		
			Maximum ^a	Minimum ^a	Average ^a
Carbon monoxide boiler -- Chevron (1)	2.6 ^{b, c}	9.4	14.1	10.6	12.4
Coke kilns -- Great Lakes Carbon (3)	2.8 ^{b, c} (each)	30.4	45.7	34.2	39.9
Coke kiln -- Martin Marietta Carbon (1)	2.8 ^{b, c}	10.1	15.2	11.4	13.3
Sulfuric acid units -- Stauffer Chemical (3)	0.78 ^d (each)	8.5	12.8	9.6	11.2
Total	--	--	--	--	82.6 ^e

^aMaximum based on +40 percent retrofit and +40 percent redundancy factors (see Table 65). Minimum based on +10 percent retrofit and +10 percent redundancy factors. Average based on +25 percent retrofit and +25 percent redundancy factors.

^bDouble alkali process

^cIncludes \$100,000 for reheat heat exchanger estimated from Ref. 10. Adjusted to late 1977 dollars.

^dLime scrubbing process

^eMaximum retrofit and redundancy factors used for Great Lakes Carbon installation because of installation complexity

TABLE 11. SULFUR DIOXIDE SCRUBBER COST SUMMARY
Average costs in late 1977 dollars

Installation and No. of units	Total capital investment		Annualized cost, ^a including disposal			Approximate product selling price, \$	Percent of selling price
	Millions of dollars ^{b,c}	\$/kW	\$/ton sulfur dioxide removed	mills/kWh or \$/ton of product	Millions of dollars		
Electrical utility sites -- SCE and DWP units (8)	1,363	135	3,612 ^d	8.8 mills ^d	339.3	--	--
Carbon monoxide boiler -- Chevron (1)	12.4	--	3,200 ^{e,f}	7.8 mills ^{e,f}	300.7 ^e	45 ^g 35 ^h	17 22
Coke kilns -- Great Lakes Carbon (3)	45.7	--	3,440	Not applic- able	3.2	--	--
Coke kiln -- Martin Marietta Carbon (1)	13.3	--	2,415	\$19.72	11.7	110	18
Sulfuric acid units Stauffer Chemical (3)	11.2	--	1,140	\$13.93	3.5	110	13
			5,544	\$10.23	2.7	50	20

^aBased on 20-year lifetime of facility

^bAverage value, see Section 4.5.1.1

^cMaximum retrofit and redundancy factors applied (+40 percent, each) because of installation complexity (others +25 percent, each)

^dExcluding SCE Redondo Beach Units 1 through 4 and DWP Valley Station. Both are age limited (assumed as 10 yr): annualized costs 32 mills/kWh

^eIncludes 1.0 mill/kWh credit from use of 0.5 percent sulfur oil at \$0.70 per barrel less than 0.25 percent sulfur oil

^f7.8 mills/kWh equivalent to \$5.59/bbl, or \$0.91 per million Btu input

^gDomestic service rate

^hGeneral service rate

be reduced to 7.8 mills/kWh or \$3200 per ton of SO₂ removed (Table 11). These costs, however, do not include costs incurred as a result of shutdown of the operating units during scrubber installation.

Comparable annual costs for 20-year life industrial process scrubbers range from \$1140 to \$5544 per ton of SO₂ removed. Other comparisons are shown in Table 11.

For industrial process scrubbers, the effect of paying for scrubber equipment at a faster rate than the 20-year lifetime was determined. If emission source capacity factors remained unchanged, amortizing the capital equipment costs in 5 years instead of 20 would increase the annualized costs by a factor of 1.59.

The effect of remaining life and capacity factor of an electrical generating facility is illustrated by assessing the effect of a 10-year life on the SCE Redondo Units 1 through 4 and the DWP Valley plant. These are old installations and operate at low capacity factors of approximately 15 percent as contrasted to approximately 42 percent for the other units in the study. The average operating cost increases from 8.8 mills/kWh to 31.6 mills/kWh, or \$13,500 per ton of SO₂ removed (see Section 4.5.2 and Appendix E).

3. RECOMMENDATIONS

Inasmuch as installation of sulfur dioxide (SO_2) scrubbers on specific units in the Los Angeles area has been shown to be feasible, certain considerations are of importance regarding the effect of SO_2 scrubbing on the industry as a whole, on other environmental control systems, and on the environment itself. Therefore, it is recommended that studies be conducted as follows:

- a. Determine the feasibility of installing SO_2 scrubbers on other major stationary sources of emissions such as industrial boilers, primary metals and glass furnaces, sulfur recovery units, petroleum process heaters, and oil field recovery vapor phase reactors.
- b. Determine the effect of wet SO_2 scrubbers on the formation of SO_3 and on SO_3 acid mist emissions.
- c. With SO_2 and NO_x control devices operating simultaneously on utility and other boilers, determine their impact on the feasibility of installation, the interactions of the two systems, the reliability of operation of each control system and of the combined systems, and the total environmental control costs for systems to meet prescribed standards.

